

# A 0.9-V, 150-MHz, 10-mW, 4 mm<sup>2</sup>, 2-D Discrete Cosine Transform Core Processor with Variable Threshold-Voltage (VT) Scheme

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**Abstract**—A 4 mm<sup>2</sup>, two-dimensional (2-D) 8 × 8 discrete cosine transform (DCT) core processor for HDTV-resolution video compression/decompression in a 0.3-μm CMOS triple-well, double-metal technology operates at 150 MHz from a 0.9-V power supply and consumes 10 mW, only 2% power dissipation of a previous 3.3-V design. Circuit techniques for dynamically varying threshold voltage (VT scheme) are introduced to reduce active power dissipation with negligible overhead in speed, standby power dissipation, and chip area. A way to explore  $V_{DD} - V_{th}$  design space is also studied.

## I. INTRODUCTION

LOWERING both the supply voltage  $V_{DD}$  and threshold voltage  $V_{th}$  enables high-speed, low-power operation [1], [2]. This approach, however, raises two problems [3], [4], 1) degradation of worst-case speed due to  $V_{th}$  fluctuation in low  $V_{DD}$ , and 2) increase in standby power dissipation in low  $V_{th}$ . To solve these problems, several schemes are proposed. A self-adjusting threshold voltage (SAT) scheme [5] reduces  $V_{th}$  fluctuation in an active mode by adjusting substrate bias with a feedback control circuit. A standby power reduction (SPR) scheme [6] raises  $V_{th}$  in a standby mode by switching substrate bias between the power supply and an external additional supply higher than  $V_{DD}$  or lower than GND. A multi threshold voltage CMOS (MT-CMOS) scheme [7] employ low  $V_{th}$  for fast circuit operation and high  $V_{th}$  for providing and cutting internal supply voltage. The SAT and the SPR are both based upon the same idea that  $V_{th}$  is controlled dynamically through substrate bias. However, the two schemes cannot be combined because the SPR requires the external supply for the substrate bias while the SAT generates the substrate bias internally. The MT-CMOS does not solve the first problem. It requires very large transistors for the internal power supply control to impose area and yield penalties, otherwise degrading circuit speed. Furthermore, it cannot be applied to memory

elements without circuit tricks which add another area and speed penalties.

This paper presents a variable threshold voltage scheme (VT scheme) which can solve these two problems uniformly in a unified way by controlling substrate bias with substrate bias feedback control circuits. Unlike the conventional approaches, it requires no external power supply for the substrate bias, leaves no restriction in use, imposes practically no penalty in speed and chip area, and can be applied to both logic gates and memory elements. The VT scheme is employed in a two-dimensional (2-D) 8 × 8 discrete cosine transform (DCT) core processor for portable HDTV-resolution video compression/decompression. This DCT in a 0.3-μm CMOS technology operates at 150 MHz from a 0.9-V power supply and consumes 10 mW, only 2% power dissipation of a previous 3.3-V design [8].

In Section II, low  $V_{DD}$ , low  $V_{th}$  design space is explored to investigate  $V_{th}$  target. In Section III, the VT scheme is presented, followed by descriptions of circuit implementations in Section IV. Section V details the design of the DCT. Experimental results appear in Section VI. Section VII is dedicated for conclusions.

## II. EXPLORING LOW- $V_{DD}$ LOW- $V_{th}$ DESIGN SPACE

CMOS power dissipation is given by

$$P = \frac{1}{2} \cdot p_t \cdot f_{CLK} \cdot C_L \cdot V_{DD}^2 + I_0 \cdot 10^{-(V_{th}/S)} \cdot V_{DD} \quad (1)$$

where  $p_t$  is the switching probability,  $f_{CLK}$  is the clock frequency,  $C_L$  is the load capacitance,  $S$  is the subthreshold swing, and  $I_0$  is a constant which is proportional to total transistor width in a chip. The first term represents dynamic power dissipation due to charging and discharging of the load capacitance, and the second term is leakage current dissipation due to subthreshold conduction. Since the dominant term in a typical CMOS design is the dynamic power dissipation, lowering  $V_{DD}$  is effective to low-power design.

Gate propagation delay, on the other hand, is approximately given in [9] by

$$t_{pd} = \frac{k \cdot C_L \cdot V_{DD}}{(V_{DD} - V_{th})^\alpha} \quad (2)$$

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where  $\alpha$  is typically 1.3 and  $k$  is a constant. Lowering only  $V_{DD}$  leads to slower circuit speed, and therefore, both of  $V_{DD}$  and  $V_{th}$  should be lowered for high-speed, low-power design. When  $V_{DD}$  and  $V_{th}$  are lowered to  $V'_{DD}$  and  $V'_{th}$ , and the circuit speed becomes  $\lambda$  times, their relation is given from (2) by

$$\frac{V'_{DD} - V'_{th}}{V_{DD} - V_{th}} = \left( \lambda \cdot \frac{V'_{DD}}{V_{DD}} \right)^{1/\alpha}. \quad (3)$$

For example, suppose  $V_{DD} = 3.3$  V and  $V_{th} = 0.6$  V. Under a constant speed condition ( $\lambda = 1$ ), one solution is  $V'_{DD} = 2.1$  V and  $V'_{th} = 0.2$  V. In this case, the dynamic power dissipation is reduced to 41%. If circuit speed can be reduced to 60% ( $\lambda = 0.6$ ), the dynamic power dissipation can be reduced to 7% at  $V'_{DD} = 0.9$  V and  $V'_{th} = 0.2$  V.

For more precise estimation, process fluctuation should be taken into account.  $V_{th}$  fluctuates typically by  $\pm 0.1$  V, which causes  $t_{pd}$  variation. From (2), the variation in  $t_{pd}$ ,  $K_{VT}$ , is given by

$$\begin{aligned} K_{VT} &= \frac{\Delta t_{pd}}{t_{pd}} \\ &= \frac{\alpha \cdot \Delta V_{th}}{V_{DD} - V_{th}}. \end{aligned} \quad (4)$$

In order to assure high yield in production, margin should be incorporated into design so as to satisfy speed specification even with fluctuations in process. Smaller  $K_{VT}$  leads to smaller design margin, and therefore, is preferable from area-saving and low-power design point of view. In lowering both  $V_{DD}$  and  $V_{th}$ ,  $K_{VT}$  should be kept at least from increasing. From (3) and (4), calculating the condition to keep  $K_{VT}$  constant yields

$$\frac{\Delta V'_{th}}{\Delta V_{th}} = \left( \lambda \cdot \frac{V'_{DD}}{V_{DD}} \right)^{1/\alpha}. \quad (5)$$

In the former examples, under the constant speed condition ( $\lambda = 1$ )  $V_{th}$  fluctuation should be reduced to  $\Delta V'_{th}/\Delta V_{th} = 0.71$ , and in the 60%-speed condition ( $\lambda = 0.6$ ) it should be reduced to  $\Delta V'_{th}/\Delta V_{th} = 0.25$ .

But in reality, it is not expected that as  $V_{th}$  is lowered,  $\Delta V_{th}$  is reduced as much. If impurity density in the channel region is simply reduced to lower  $V_{th}$  of a surface channel device such as nMOS with n<sup>+</sup> polysilicon gates, the short-channel effect degrades to increase  $\Delta V_{th}$ , reflecting variation of polysilicon gates in size. In a buried-channel device such as pMOS with n<sup>+</sup> polysilicon gates, on the other hand, counter doping should be added to lower  $V_{th}$ , resulting in higher impurity density and larger  $\Delta V_{th}$ . It is not that simple to discuss  $\Delta V_{th}$ , but generally speaking, device researchers expect  $\Delta V_{th}$  could be increased in low  $V_{th}$  and would not be decreased very easily. This is one issue in low- $V_{DD}$ , low- $V_{th}$  CMOS circuit design.

Another issue is the rapid increase in subthreshold leakage in low  $V_{th}$  as seen from (1). In portable applications it is clear that large standby leakage becomes a problem. Not only in portable applications but also in desktop applications, the rapid increase in subthreshold current determines the lower limit of  $V_{th}$ , and therefore, it is also important.

In order to study these two issues and explore low- $V_{DD}$ , low- $V_{th}$  design space, (1) and (2) are numerically solved with the parameters for this DCT design in a 0.3- $\mu$ m CMOS technology at junction temperature of 90°C. Contour lines in terms of speed (i.e., maximum operating frequency) and power are drawn on the  $V_{DD} - V_{th}$  plane in Fig. 1. In a typical 3.3-V design,  $V_{DD}$  is at  $3.3 \pm 10\%$  V and  $V_{th}$  is set to  $0.6 \pm 0.1$  V. The design space is represented by a box in Fig. 1. The maximum operating frequency,  $f$ , becomes the slowest, 250 MHz, at  $V_{DD} = 3.0$  V and  $V_{th} = 0.7$  V. The circuit speed is therefore normalized ( $\lambda = 1$ ) at the upper-left corner of the design-space box. The power dissipation, on the other hand, becomes the largest, 160 mW, at  $V_{DD} = 3.6$  V and  $V_{th} = 0.5$  V. The power dissipation is therefore normalized ( $\xi = 1$ ) at the lower-right corner of the design-space box. For designing a 150 MHz DCT, which is 60% speed of 250 MHz, the upper-left corner of the design-space box should be placed on the speed contour line with  $\lambda = 0.6$ . It is found from the lower-right corner of the design-space box that the power dissipation can be reduced to 25% ( $\xi = 0.25$ ), that is 40 mW, by lowering  $V_{DD}$  to  $1.9 \pm 10\%$  V. It can further be reduced to 6% ( $\xi = 0.06$ ), that is 10 mW, by lowering both  $V_{DD}$  to  $1.0 \pm 10\%$  V and  $V_{th}$  to  $0.27 \pm 0.02$  V. This supply voltage can be supplied from a single battery source. Reducing  $\Delta V_{th}$  from  $\pm 0.1$  V to  $\pm 0.02$  V also meets the requirement for keeping  $K_{VT}$  constant in (5). As shown in Fig. 1, power dissipation due to subthreshold leakage becomes about 1% of the total power dissipation.

To summarize,  $V_{DD}$  should be at  $1.0 \pm 10\%$  V, and  $V_{th}$  should be controlled at  $0.27 \pm 0.02$  V in the active mode and higher than 0.5 V in the standby mode.

### III. VARIABLE THRESHOLD-VOLTAGE (VT) SCHEME

The VT scheme is conceptually illustrated in Fig. 2. Threshold voltage of a transistor is variable through substrate bias control with a Variable Threshold-voltage circuit (VT circuit). In the active mode, the VT circuit controls the substrate bias,  $V_{BB}$ , so as to compensate the  $V_{th}$  fluctuation. Even though device  $V_{th}$  has 0.1-V fluctuation around 0.15 V,  $V_{th}$  is compensated and set at  $0.27 \pm 0.02$  V in the active mode. In the standby mode, the VT circuit applies deeper substrate bias to increase  $V_{th}$  to higher than 0.5 V and cut off leakage. Typically,  $V_{BB}$  of  $-0.5$  V is applied in the active mode and  $-3.3$  V in the standby mode.

Fig. 3 depicts the VT scheme block diagram. The VT scheme consists of four leakage current monitors (LCM's), the self-substrate bias circuit (SSB), and a substrate charge injector (SCI). The SSB draws current from the substrate to lower  $V_{BB}$ . The SCI, on the other hand, injects current into the substrate to raise  $V_{BB}$ . The SSB and the SCI are controlled by monitoring where  $V_{BB}$  sits in four ranges. Their criteria are specified in the four LCM's;  $V_{\text{active}(+)} = -0.3$  V,  $V_{\text{active}} = -0.5$  V,  $V_{\text{active}(-)} = -0.7$  V, and  $V_{\text{standby}} = -3.3$  V. The substrate bias is monitored by transistor leakage current, because the leakage current reflects  $V_{BB}$  very sensitively.

Fig. 4 illustrates the substrate bias control. After a power-on,  $V_{BB}$  is higher than  $V_{\text{active}(+)}$ , and the SSB begins to draw

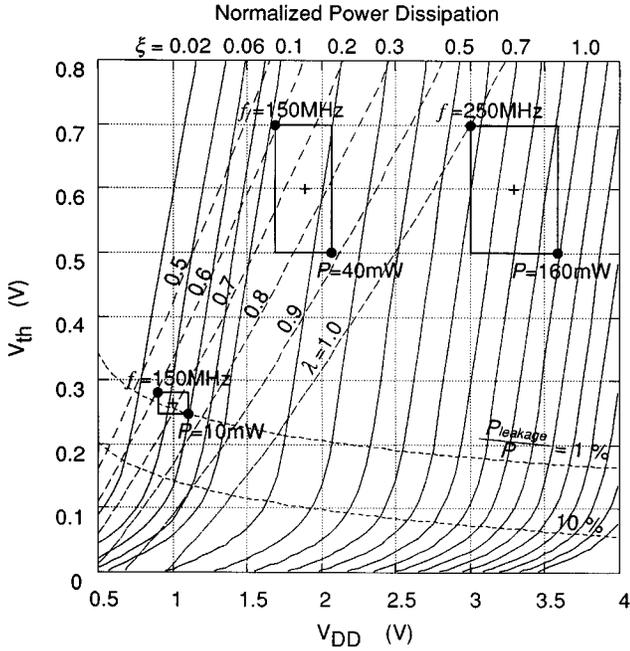


Fig. 1. Exploring low- $V_{DD}$ , low- $V_{th}$  design space. Contour lines in terms of speed (broken lines) and power (solid lines) are drawn.

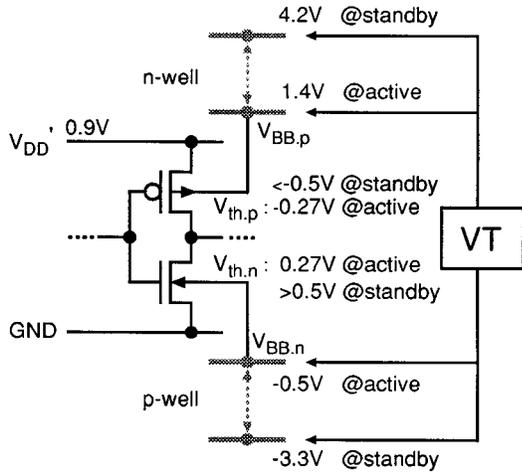


Fig. 2. Variable threshold-voltage (VT) scheme.

100  $\mu$ A from the substrate to lower  $V_{BB}$  using a 50 MHz ring oscillator. This current is large enough for  $V_{BB}$  to settle down within 10  $\mu$ s after a power-on. When  $V_{BB}$  goes lower than  $V_{active(+)}$ , the pump driving frequency drops to 5 MHz and the SSB draws 10  $\mu$ A to control  $V_{BB}$  more precisely. The SSB stops when  $V_{BB}$  drops below  $V_{active}$ .  $V_{BB}$ , however, rises gradually due to device leakage current through MOS transistors and junctions, and reaches  $V_{active}$  to activate the SSB again. In this way,  $V_{BB}$  is controlled at  $V_{active}$  by the on-off control of the SSB. When  $V_{BB}$  goes deeper than  $V_{active(-)}$ , the SCI turns on to inject 30 mA into the substrate. Therefore, even if  $V_{BB}$  jumps beyond  $V_{active(+)}$  or  $V_{active(-)}$  due to a power line bump for example,  $V_{BB}$  is quickly recovered to  $V_{active}$  by the SSB and the SCI. When “SLEEP” signal is asserted (“1”) to go to the standby mode, the SCI is disabled and the SSB is activated again and 100  $\mu$ A current is

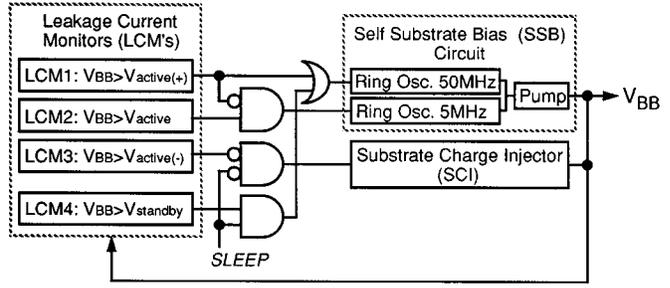


Fig. 3. VT block diagram.

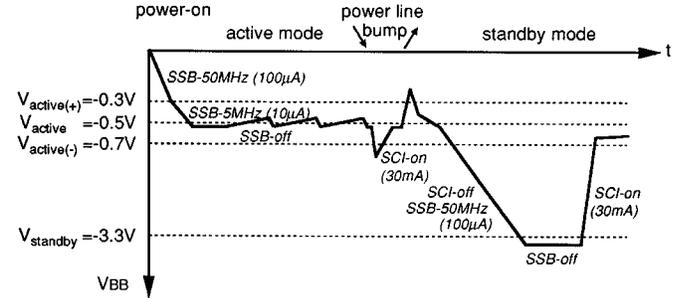


Fig. 4. Substrate-bias control in VT.

drawn from the substrate until  $V_{BB}$  reaches  $V_{standby}$ .  $V_{BB}$  is controlled at  $V_{standby}$  in the same way by the on-off control of the SSB. When “SLEEP” signal becomes “0” to go back to the active mode, the SSB is disabled and the SCI is activated. The SCI injects 30 mA current into the substrate until  $V_{BB}$  reaches  $V_{active(-)}$ .  $V_{BB}$  is finally set at  $V_{active}$ . In this way, the SSB is mainly used for a transition from the active mode to the standby mode, while the SCI is used for a transition from the standby to the active mode. An active to standby mode transition takes about 100  $\mu$ s, while a standby to active mode transition is completed in 0.1  $\mu$ s. This “slow falling asleep but fast awakening” feature is acceptable for most of the applications.

The SSB operates intermittently to compensate for the voltage fluctuation in the substrate due to the substrate current in the active and the standby modes. It therefore consumes several microamperes in the active mode and less than one nanoampere in the standby mode, both much lower than the chip power dissipation. Energy required to charge and discharge the substrate for switching between the active and the standby modes is less than 10 nJ. Even when the mode is switched 1000 times in a second, the power dissipation becomes only 10  $\mu$ W. The leakage current monitor should be designed to dissipate less than 1 nA because it always works even in the standby mode. The low-power circuit design technique is described in the next section.

IV. CIRCUIT IMPLEMENTATIONS

A. Leakage Current Monitor (LCM)

The substrate bias is generated by the SSB which is controlled by the leakage current monitor (LCM). The LCM is therefore a key to the accurate control in the VT scheme. Fig. 5

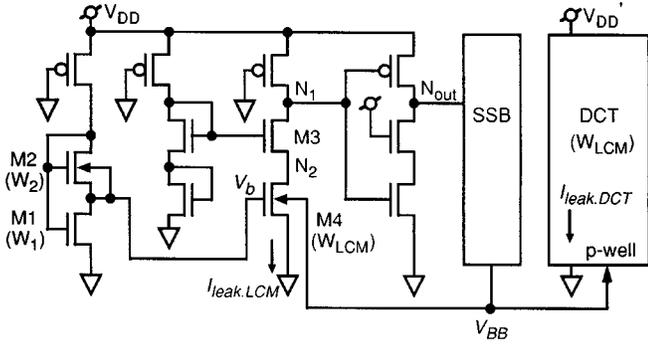


Fig. 5. Leakage current monitor (LCM).

depicts a circuit schematic of the proposed LCM. The circuit works with 3.3-V  $V_{DD}$  which is usually available on a chip for standard interfaces with other chips. The LCM monitors leakage current of the DCT,  $I_{leak.DCT}$ , with a transistor M4 that shares the same substrate with the DCT. The gate of M4 is biased to  $V_b$  to amplify the monitored leakage current,  $I_{leak.LCM}$ . If  $I_{leak.LCM}$  is larger than a target reflecting shallower  $V_{BB}$  and lower  $V_{th}$ , the node  $N_1$  goes “Low” and the output node  $N_{out}$  goes “High” to activate the SSB. As a result,  $V_{BB}$  goes deeper and  $V_{th}$  becomes higher, and consequently,  $I_{leak.LCM}$  and  $I_{leak.DCT}$  become smaller. When  $I_{leak.LCM}$  becomes smaller than the target, the SSB stops. Then  $I_{leak.LCM}$  and  $I_{leak.DCT}$  increase as  $V_{BB}$  gradually rises due to device leakage current through MOS transistors and junctions, and finally reaches the target to activate the SSB again. In this way,  $I_{leak.DCT}$  is set to a target by the on-off control of the SSB with the LCM.

In order to make this feedback control accurately, the current ratio of  $I_{leak.LCM}$  to  $I_{leak.DCT}$ , or the current magnification factor of the LCM,  $X_{LCM}$ , should be constant. When an MOS transistor is in subthreshold, its drain current is expressed as

$$I_{DS} = \frac{I_0}{W_0} \cdot W \cdot 10^{(V_{GS}-V_T)/S} \quad (6)$$

where  $S$  is the subthreshold swing,  $V_T$  is the threshold voltage,  $I_0/W_0$  is the current density to define  $V_T$ , and  $W$  is the channel width. By applying (6),  $X_{LCM}$  is given by

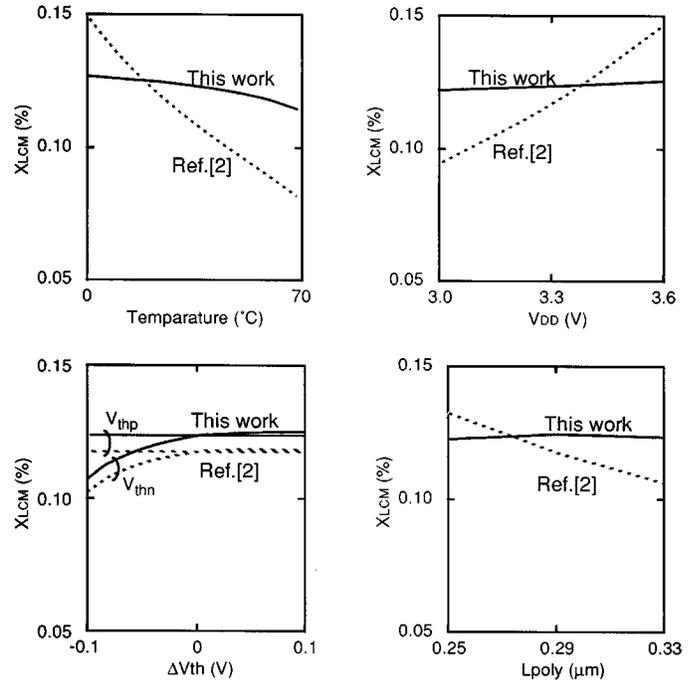
$$\begin{aligned} X_{LCM} &= \frac{I_{leak.LCM}}{I_{leak.DCT}} \\ &= \frac{W_{LCM}}{W_{DCT}} \cdot 10^{V_b/S} \end{aligned} \quad (7)$$

where  $W_{DCT}$  is the total channel width of the DCT and  $W_{LCM}$  is the channel width of M4. Since two transistors M1 and M2 in a bias generator are designed to operate in subthreshold region, the output voltage of the bias generator  $V_b$  is also given from (6) by

$$V_b = S \cdot \log \frac{W_2}{W_1} \quad (8)$$

where  $W_1$  and  $W_2$  is the channel width of M1 and M2, respectively.  $X_{LCM}$  is therefore expressed as

$$X_{LCM} = \frac{W_2}{W_1} \cdot \frac{W_{LCM}}{W_{DCT}}. \quad (9)$$


 Fig. 6. Current magnification factor of the LCM,  $X_{LCM}$ , dependence on circuit condition changes and process deviations simulated by SPICE.

This implies that  $X_{LCM}$  is determined only by the transistor size ratio and independent of the power supply voltage, temperature, and process fluctuation. In the conventional circuit [5], on the other hand, where  $V_b$  is generated by dividing the  $V_{DD}$ -GND voltage with high impedance resistors,  $V_b$  becomes a function of  $V_{DD}$ , and therefore,  $X_{LCM}$  becomes a function of  $V_{DD}$  and  $S$ , where  $S$  is a function of temperature. Fig. 6 shows SPICE simulation results of  $X_{LCM}$  dependence on circuit condition changes and process fluctuation.  $X_{LCM}$  exhibits small dependence on  $\Delta V_{thn}$  and temperature. This is because M4 is not in deep subthreshold region. The variation of  $X_{LCM}$ , however, is within 15%, which results in less than 1% error in  $V_{th}$  controllability. This is negligible compared to 20% error in the conventional implementation.

The four criteria used in the substrate-bias control, corresponding to  $V_{active(+)}$ ,  $V_{active}$ ,  $V_{active(-)}$ , and  $V_{standby}$  can be set in the four LCM's by adjusting the transistor size  $W_1$ ,  $W_2$ , and  $W_{LCM}$  in the bias circuit. For the active mode, with  $W_1 = 10 \mu\text{m}$ ,  $W_2 = 100 \mu\text{m}$ , and  $W_{LCM} = 100 \mu\text{m}$ , the magnification factor  $X_{LCM}$  of 0.001 is obtained when  $W_{DCT} = 1 \text{ m}$ .  $I_{leak.DCT}$  of 0.1 mA can be monitored as  $I_{leak.LCM}$  of 0.1  $\mu\text{A}$  in the active mode. For the standby mode, with  $W_1 = 10 \mu\text{m}$ ,  $W_2 = 1000 \mu\text{m}$ , and  $W_{LCM} = 1000 \mu\text{m}$ ,  $X_{LCM}$  becomes 0.1. Therefore,  $I_{leak.DCT}$  of 10 nA can be monitored as  $I_{leak.LCM}$  of 1 nA in the standby mode. The overhead in power by the monitor circuit is about 0.1 and 10% of the total power dissipation in the active and the standby mode, respectively.

The parasitic capacitance at the node  $N_2$  is large because M4 is large. This may degrade response speed of the circuit. The transistor M3, however, isolates the  $N_1$  node from the  $N_2$  node and keeps the signal swing on  $N_2$  very small. This reduces the response delay and improves dynamic  $V_{th}$  controllability.

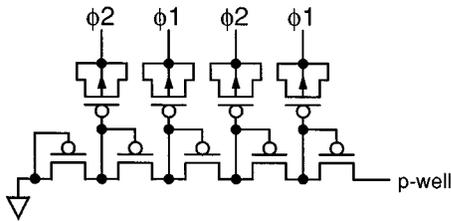


Fig. 7. Pump circuit in SSB.

Compared with the conventional LCM where  $V_b$  is generated by dividing the  $V_{DD}$ -GND voltage with high impedance resistors, the  $V_{th}$  controllability including the static and dynamic effects is improved from  $\pm 0.05$  V to less than  $\pm 0.01$  V, response delay is shortened from 0.6 to 0.1  $\mu$ s, and Si area is reduced from 33 250 to 670  $\mu$ m<sup>2</sup>. This layout area reduction is brought by the elimination of the high impedance resistors by polysilicon.

### B. Self-Substrate Bias Circuit (SSB)

Fig. 7 depicts a schematic diagram of a pump circuit in the SSB. PMOS transistors of the diode configuration are connected in series whose intermediate nodes are driven by two signals,  $\Phi 1$  and  $\Phi 2$ , in 180° phase shift. Every other transistor, therefore, sends current alternately from p-well to GND, resulting in lower p-well bias than GND. The SSB can pump as low as  $-4.5$  V. SSB circuits are widely used in DRAM's and E<sup>2</sup>PROM's, but two orders of magnitude smaller circuit can be used in the VT scheme. The driving current of the SSB is 100  $\mu$ A, while it is usually several milliamperes in DRAM's. This is because substrate current generation due to the impact ionization is a strong function of the supply voltage. Substrate current in a 0.9-V DCT is considerably smaller than that in a 3.3-V design. Substrate current introduced from I/O pads does not affect the DCT macro because it is separated from peripheral circuits by a triple-well structure. Eventually, no substrate current is generated in the standby mode. From these reasons, the pumping current in the SSB can be as small as several percent of that in DRAM's. Silicon area is also reduced considerably. Another concern about the SSB is an initialization time after a power-on. Even in a 10 mm square chip,  $V_{BB}$  settles down within 200  $\mu$ s after a power-on, which is acceptable in real use.

### C. Substrate Charge Injector (SCI)

In the VT scheme, care should be taken so that no transistor sees high-voltage stress of gate oxide and junctions. Transistors are optimized for use at 3.3 V. The gate oxide thickness is 8 nm. The maximum voltage that assures sufficient reliability of the gate oxide is  $V_{DD} + 20\%$ , or 4 V. The SCI in Fig. 8 receives a control signal that swings between  $V_{DD}$  and GND at node  $N_1$  to drive substrate from  $V_{standby}$  to  $V_{active}$ . In the standby-to-active transition,  $V_{DD} + |V_{standby}|$  that is about 6.6 V at maximum can be applied between  $N_1$  and  $N_2$ . However, as shown in SPICE simulated waveforms in Fig. 8,  $|V_{GS}|$  and  $|V_{GD}|$  of M1 and M2 never exceeds the larger of  $V_{DD}$  and  $|V_{standby}|$ . All other transistors in the VT circuit and

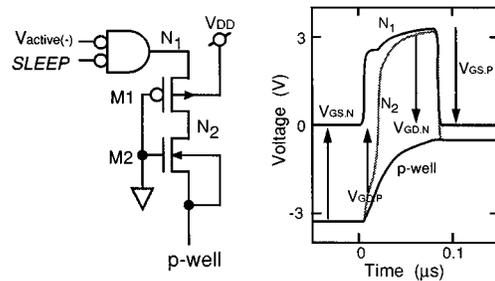


Fig. 8. SCI and its waveforms simulated by SPICE.

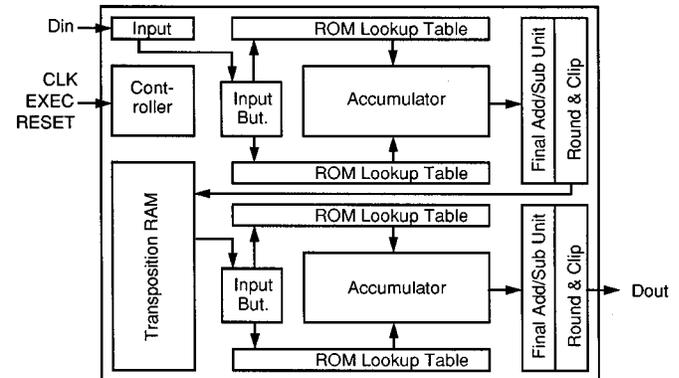


Fig. 9. DCT block diagram.

the DCT macro receive  $(V_{DD} - V_{th})$  on their gate oxide when the channel is formed in the depletion and the inversion mode, and less than  $|V_{standby}|$  in the accumulation mode. These considerations lead to a general guideline that  $V_{standby}$  should be limited to  $-(V_{DD} + 20\%)$ .  $V_{standby}$  of  $-(V_{DD} + 20\%)$ , however, can shift  $V_{th}$  big enough to reduce the leakage current in the standby mode. The body effect coefficient,  $\gamma$ , can be adjusted independently to  $V_{th}$  by controlling the doping concentration density in the channel-substrate depletion layer.

## V. DCT DESIGN

### A. Circuit Design

This DCT core processor executes 2-D  $8 \times 8$  DCT and inverse DCT. A block diagram is illustrated in Fig. 9. The DCT is composed of two one-dimensional (1-D) DCT and inverse DCT processing units and a transposition RAM. Rounding circuits and clipping circuits which prevent overflow and underflow are also implemented in the cell. The DCT has a concurrent architecture based on distributed arithmetic and a fast DCT algorithm, which enables high throughput DCT processing of one pixel per clock. It also has fully pipelined structure. The 64 input data sampled in every clock cycles are outputted after 112 clock cycle latency.

Various memories which use the same low  $V_{th}$  transistors as logic gates are employed in the DCT. Table lookup ROM's (16 b  $\times$  32 words  $\times$  16 banks) employ contact programming and an inverter-type sense-amplifier. Single-port SRAM's (16 b  $\times$  64 words  $\times$  2 banks) and dual-port SRAM's (16 b  $\times$  8 words  $\times$  2 banks) employ a six-transistor cell and a latch sense-amplifier. They all exhibit wide operational margin in

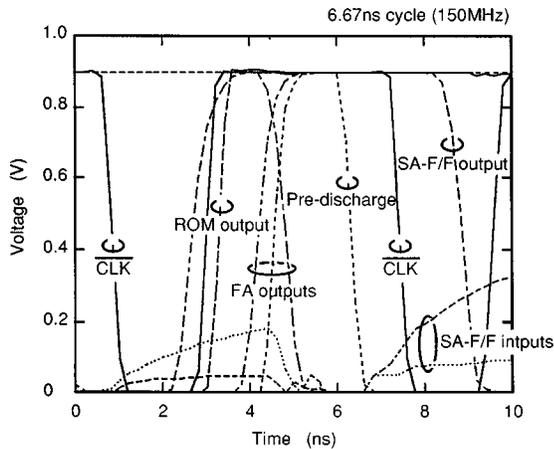


Fig. 10. Simulated waveforms of MAC datapath.

low  $V_{DD}$  and low  $V_{th}$  and almost behave like logic gates in terms of circuit speed dependence on  $V_{DD}$  and  $V_{th}$ . No special care is necessary such as word-line boosted-up or a special sense-amplifier.

Small-swing differential pass-transistor logic (SAPL) with sense-amplifying pipeline flip-flop (SA-F/F) [8] is employed for high-speed operation in a 20-b carry skip adder in an accumulator. The SAPL operates and maintains its speed advantage at 0.9 V because the SA-F/F uses a current-mode latch sense-amplifier. As shown in SPICE simulation in Fig. 10, a multiplication and accumulation (MAC) datapath runs at 150 MHz under 0.9 V with no modifications from the 3.3-V design [8].

### B. Layout Design

In the conventional CMOS, substrate-contacts are connected to power lines locally, while in the VT scheme they should be interconnected globally for biasing the substrate. This may impose area penalty for separating many substrate contacts, or performance degradation due to substrate noise with few substrate contacts. It is considered, however, that not many substrate contacts are needed in 0.9-V design compared to 3.3-V design because the substrate current generated by the impact ionization becomes several orders of magnitude smaller in 0.9 V. As for substrate noise induced by drain-substrate capacitive coupling, lowering supply voltage is favorable because signal swing as a noise source becomes smaller. It should be effective to add source diffusions because it helps to stabilize  $V_{BB}$  by junction capacitance between source diffusions and substrate.

Layout design of the DCT is made in the conventional CMOS fashion, and then it is automatically modified for the VT scheme as illustrated in Fig. 11 by a script of a layout editor. First, have the DCT macro wrapped by deep n-well. Second, generate p-well by inverting n-well data in the deep n-well. Third, replace all the substrate-contacts by source diffusions as long as design rules accept, otherwise remove them. Lastly, place substrate-contacts at the periphery of the deep n-well and the p-well. The p-well becomes one big island and can be connected at periphery. The n-well, on the other hand, becomes many pieces of separated islands.

However, they sit in one deep n-well and can be connected at the periphery, too. Since substrate contacts are only placed at periphery of the 2 mm-square macro, large parasitic substrate resistance is included. Performance degradation or latch up effect due to substrate noise should be examined. Experimental results are presented in the next section. The area penalty, on the other hand, becomes less than 0.1%. This can be done in a p-well or an n-well technology, too, but triple-well structure prevents I/O noise from affecting the DCT macro. The increase in cost and turnaround time by introducing triple-well process is less than 5%. The necessity of the triple-well structure should be examined in the future.

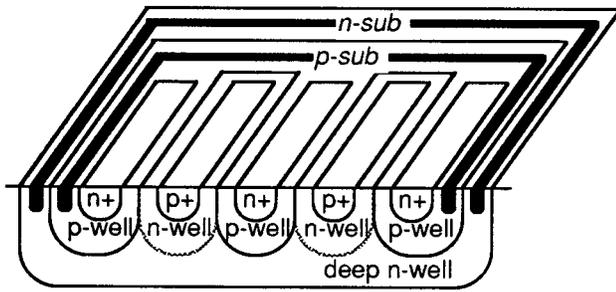
## VI. EXPERIMENTAL RESULTS

The DCT core processor is fabricated in a 0.3- $\mu\text{m}$  CMOS, triple-well, double-metal technology. Parameters of the technology and the features of the DCT macro are summarized in Table I. It operates with 0.9-V power supply which can be supplied from a single battery source. Power dissipation at 150 MHz operation is 10 mW. The leakage current in the active mode is 0.1 mA, about 1% of the total power current. The standby leakage current is less than 10 nA, four orders of magnitude smaller than the active leakage current. A chip micrograph appears in Fig. 12(a). The core size is 2 mm square. A magnified picture of the VT control circuit appears in Fig. 12(b). It occupies 0.37 mm  $\times$  0.52 mm, less than 5% of the macro size. If additional circuits for testability are removed and the layout is optimized, the layout size is estimated to be 0.3 mm  $\times$  0.3 mm. The VT circuit is symmetric for p-well and n-well control. LCM(N), however, occupies more area than LCM(P) because nMOS transistor loads in LCM(N) need longer gate length than pMOS transistor loads in LCM(P) for monitoring the same  $I_{\text{leak,LCM}}$ .

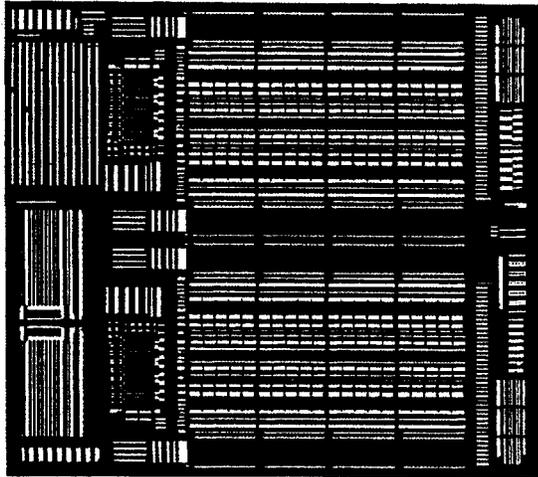
Fig. 13(a)–(c) shows measured p-well voltage waveforms. Due to large parasitic capacitance in a probe card, the transition takes longer time than SPICE simulation. Just after the power-on, the VT circuits are not activated yet because the power supply is not high enough. As shown in Fig. 13(a), p-well is biased forward by 0.2 V due to capacitance coupling between p-well and power lines. Then the VT circuits are activated and p-well is to be biased at  $-0.5$  V. It takes about 8  $\mu\text{s}$  to be ready for the active mode after the power-on. The active-to-standby mode transition takes about 120  $\mu\text{s}$  as shown in Fig. 13(b), while the standby-to-active mode transition is completed within 0.2  $\mu\text{s}$  as presented in Fig. 13(c).

Compared to the DCT in [8], power dissipation at 150 MHz operation is reduced from 500 mW to 10 mW, that is only 2%. Most of the power reduction, however, is brought by capacitance reduction and voltage reduction by technology scaling. Technology scaling from 0.8 to 0.3  $\mu\text{m}$  reduces power dissipation from 500 to 100 mW at 3.3 V and 150 MHz operation. Without the VT scheme,  $V_{DD}$  and  $V_{th}$  cannot be lowered under 1.7 and 0.5 V, respectively, and the active power dissipation is to be 40 mW. It is therefore fair to claim that the VT scheme contributes to reduce the active power dissipation from 40 to 10 mW.

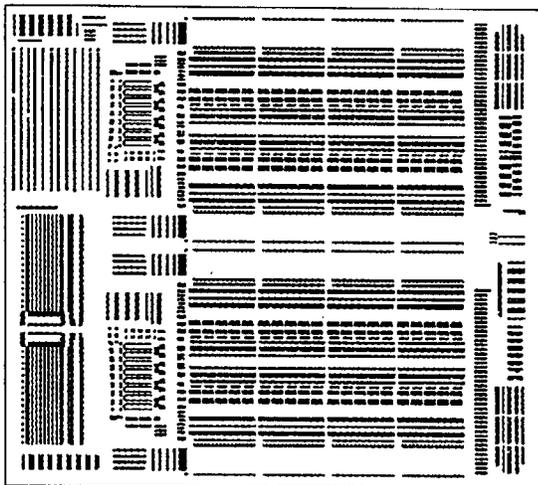
The DCT operates at supply voltages from 0.9 to above 3 V. No performance degradation nor latchup effect is observed



(a)



(b)



(c)

Fig. 11. DCT layout modification for the VT scheme: (a) device cross-section, (b) p-well (one island), and (c) n-well (pieces of islands) in deep n-well.

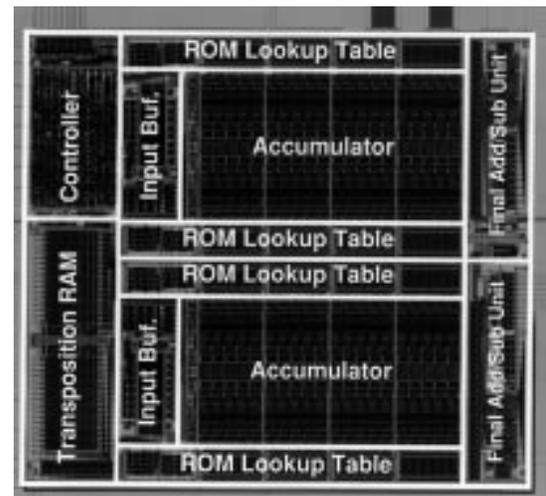
even when  $100\text{ k}\Omega$  resistance is added between the substrate and the output of the SSB.

## VII. CONCLUSIONS

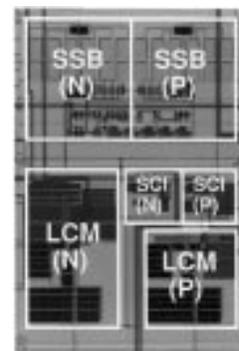
A  $4\text{ mm}^2$  2-D DCT core processor for portable multimedia equipment with HDTV-resolution video compression and decompression has been developed in a  $0.3\text{-}\mu\text{m}$  CMOS, triple-well, double-metal technology. It operates at 150 MHz from

TABLE I  
FEATURES

Technology	$0.3\text{ }\mu\text{m}$ CMOS, triple-well, double-metal, $T_{ox} = 8\text{ nm}$ , $V_{th} = 0.15\text{ V} \pm 0.1\text{ V}$
Power supply voltage	$1.0\text{ V} \pm 0.1\text{ V}$
Power dissipation	$10\text{ mW}$ @ 150 MHz
Standby current	$<10\text{ nA}$ @ $70^\circ\text{C}$
Transistor count	120K Tr
Area	$2.0 \times 2.0\text{ mm}^2$
Function	$8 \times 8$ DCT and inverse DCT
Data format	9-b signed (pixel), 12-b signed (DCT)
Latency	112 clocks
Throughput	64 clocks/block
Accuracy	CCITT H.261 compatible



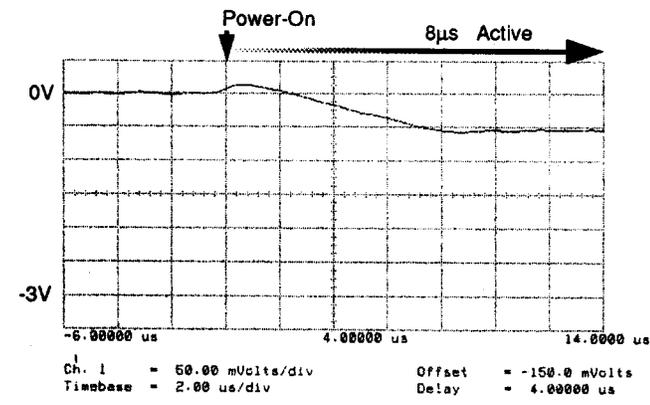
(a)



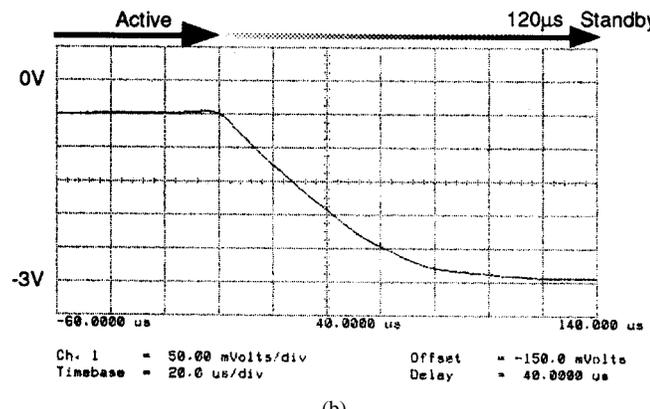
(b)

Fig. 12. Chip micrograph: (a) DCT macro and (b) VT circuits.

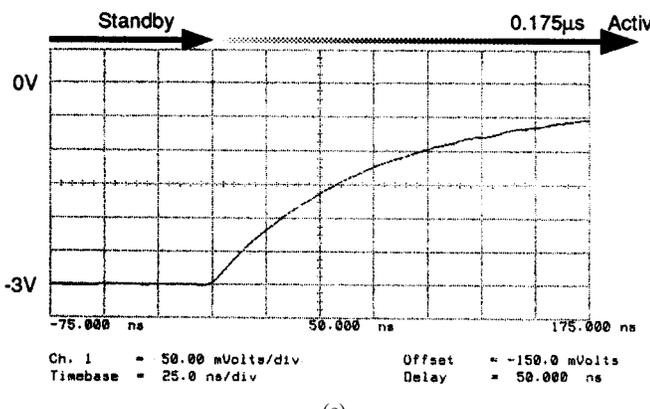
a  $0.9\text{ V}$  power supply and dissipates  $10\text{ mW}$ , which is only 2% of the previous  $3.3\text{ V}$  design. Circuit design techniques for dynamically varying threshold voltage (VT scheme) are introduced to reduce active power dissipation with negligible overhead in speed, standby power dissipation, and chip area. The active-to-standby mode transition takes  $120\text{ }\mu\text{s}$ , while the standby-to-active mode transition is completed within  $0.2\text{ }\mu\text{s}$ . The VT scheme can be applied to both logic gates and memory elements. Generation of the low-voltage  $V'_{DD}$  on chip is a future research work.



(a)



(b)



(c)

Fig. 13. Measured p-well  $V_{BB}$ : (a) after power-on, (b) active-to-standby, and (c) standby-to-active.

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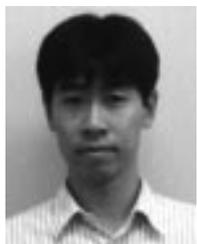
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